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CALCULATION PACKAGE

April 20, 2023

Lochwood Lozier

Lightstone Addition 5910 E. Mercer Way

Mercer Island, Washington

MULHERN & KULP STRUCTURAL ENGINEERING, INC.

Prepared By:

Riley J. Denis, E.I.T. Richard J. Zabel, P.E.

Staff Engineer Project Manager + Director of Engineering



LOCHWOOD LOZIER

LIGHTSTONE

MERCER ISLAND, WA

SHEAR WALL CALCULATIONS

REVIEWED BY: RJZ

April 13, 2023

PARAMETERS:

SINGLE FAMILY HOME

DESIGN WIND SPEED: 100 MPH

WIND EXPOSURE CATEGORY: C

Seismic Design Category: D

CODE & DESIGN STANDARD: 2018 IBC CH. 1609, ASCE 7-16 CH. 26-30





PROJECT NAME: LIGHTSTONE

M&K PROJECT #: 268-23003

ENGINEER: RJD

DATE: 13-APR-23







PROJECT NAME: LOCHWOOD LOZIER

LIGHTSTONE

M&K PROJECT #: 268-23003

Engineer: RJD Date: 13-Apr-23

SHEARWALL DESIGN SUMMARY

SHEARWALL 1ST - SIDE INTERIOR GARAGE @ EXTERIOR
SHEARWALL PROPERTIES:
Wall height, H 7.0 ft. Max wall opening ht, H _c 0.0 ft. Wall Length, L 2.0 ft. Qualifying Wall Length, L 2.0 ft. Shearwall Assembly P1
CAPACITY EVALUATION:
TOTAL SHEAR LOAD ON WALL ALLOWABLE SHEARWALL CAPACITY
SHEARWALL ASSEMBLY SPECIFICATION
P1 - 1-SIDE 7/16" OSB Fastened W/ 8d nails at 6"0.c. panel edges & 12"0.c. panel field - edges blocked <u>ADEQUATE</u>
OVERTURNING EVALUATION: Resistive DL 100 plf Overturning Moment 3.5 K-FT Hold Down Design Load 1300 lbs DL AT ENDS OF WALL 400 LBS RESISTIVE MOMENT 0.9 K-FT Hold Down Capacity 4935 LBS
HOLD-DOWN SPECIFICATION
SIMPSON STHD14RJ HOLDOWN
SHEARWALL 102: 1st - Side Interior Garge Shearwall Properties:
SHEARWALL 102: 1st - Side Interior Garge SHEARWALL PROPERTIES: Wall Height, H Wall Length, L 8.5 FT. Max wall Opening Ht, Hc Uall Length, L 12.3 FT. Qualifying Wall Length, L
SHEARWALL 102: 1st - Side Interior Garge Shearwall Properties: Wall Height, H 8.5 FT. Max Wall OPENING HT, HC 0.0 FT. Wall Length, L 12.3 FT. Qualifying Wall Length, L 12.3 FT. Shearwall Assembly P1 Capacity Evaluation: 100 100 FT. Shearwall Assembly P1
SHEARWALL 102: 1st - Side Interior Garge SHEARWALL PROPERTIES: Image: Stearwall Properties: Wall height, H 8.5 FT. Max wall opening ht, Hc 0.0 FT. Wall Length, L 12.3 FT. Qualifying Wall Length, L 12.3 FT. Capacity Evaluation: Image: Shear Load on Wall Allowable Shearwall Capacity P1 Image: Image
SHEARWALL 102: 1st - Side Interior Garge Shearwall Properties: Image: Shearwall Opening HT, Hc Image: Shearwall Assembly Wall Height, H 8.5 FT. Max wall Opening HT, Hc Image: Shearwall Assembly P1 Wall Length, L 12.3 FT. Qualifying Wall Length, L Image: Shearwall Assembly P1 Capacity Evaluation: Image: Shearwall Capacity Image: Shearwall Assembly Specification Image: Shearwall Assembly Specification Bearwall Assembly Specification Image: Shearwall Assembly Specification Image: Shearwall Assembly Specification
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SHEARWALL 102: 1st - Side Interior Garge BHEARWALL PROPERTIES: Wall Height, H 8.5 rf. Max wall opening ht, Hc 0.0 rf. Wall Length, L 12.3 rf. Qualifying Wall Length, L 12.3 rf. SHEARWALL CAPACITY 12.3 rf. Shearwall Assembly P1 Capacity Evaluation: Total Shear Load on Wall Allowable Shearwall Capacity P1 1300 LBS 4143 LBS Shearwall Capacity 1300 LBS 4143 LBS Shearwall Capacity 1300 LBS 4143 LBS Distremed w/ BD Nails at 6"0.0. Panel Assembly Specification P1 - 1-Side 7/16" DSB Assenbed w/ BD Nails at 6"0.0. Panel edgess & 12"0.0. Panel Field - edges Blooked <u>ADEQUATE</u> Distremed w/ BD Nails at 6"0.0. Panel edges & 12"0.0. Panel Field - edges Blooked <u>ADEQUATE</u> Distremed w/ BD Nails Bowent 11.1 k-ft Hold Down Design Load Lesistive DL Distremed wide use Bestrive Moment 11.3 k-ft Hold Down Design Load 0 use Los of wall
SHEARWALL 102: 1ST - SIDE INTERIOR GARGE BLEARWALL PROPERTIES: WALL HEIGHT, H 8.5 rf. MAX WALL OPENING HT, HC 0.0 rf. WALL LENGTH, L 12.3 rf. SHEARWALL ASSEMBLY P1 DEFENSION WALL LENGTH, L 0.0 rf. MAX WALL OPENING HT, HC 0.0 rf. WALL LENGTH, L 12.3 rf. SHEARWALL ASSEMBLY P1 DEFENSION WALL LENGTH, L 12.3 rf. SHEARWALL CASSEMBLY P1 DEFENSION WALL CASSEMBLY SPECIFICATION MEREWALL OSSEMBLY SPECIFICATION P1 - 1-SIDE 7/16" OSB ADEQUATE DEFENSION W/ BD NAILS AT 6"O.C. PANEL EDGES & 12"O.C. PANEL FIELD - EDGES BLOCKED DEFENSIONE W/ BD NAILS AT 6"O.C. PANEL EDGES & 12"O.C. PANEL FIELD - EDGES BLOCKED DEFENSIONE EXAMPLE MENDURATE DEFENSIONE EXAMPLE DEFENSIONE EXAMPLE DEFENSIONE EXAMPLE MENDURATE MENDURATE MENDURATE MENDURATE MENDURATE MENDURATE
SHEARWALL 102: 1st - Side Interior Garge Bischer Lander Distribution of the state of the sta

Lightstone Addition Lochwood Lozier RJD 268-23003 04-18-23

Cantilevered Retaining Wall

LIC# : KW-06017913, Build:20.23.2.14 MULHERN & KULP STRUCTURAL ENGINEERING INC

DESCRIPTION: Garage Retaining Wall

Code Reference

Calculations per IBC 2018 1807.3, CBC 2019, ASCE 7-16

Criteria

Soil Data

Retained Height	=	6.00 ft
Wall height above soil	=	0.00 ft
Slope Behind Wall	=	0.00
Height of Soil over Toe	=	0.00 in
Water height over heel	=	0.0 ft

_		_	
Surd	:har	ae L	oads

Surcharge Over Heel = 0.0 psf Used To Resist Sliding & Overturning Surcharge Over Toe = 0.0 psf Used for Sliding & Overturning Axial Load Applied to Stem					
Axial Dead Load Axial Live Load Axial Load Eccentricity	= = =	0.0 lbs 0.0 lbs 0.0 in			

Earth Pressure Seismic Load

Method : Uniform Multiplier Used 7.000 = (Multiplier used on soil density)

Allow Soil Bearing Equivalent Fluid Pressure	= Meth	2,000.0 od	psf
Active Heel Pressure	=	35.0	psf/ft
	=		
Passive Pressure	=	250.0	psf/ft
Soil Density, Heel	=	110.00	pcf
Soil Density, Toe	=	110.00	pcf
Footing Soil Friction	=	0.400	
Soil height to ignore for passive pressure	=	12.00	in

Lateral Load Applied to Stem

Lateral Load Height to Top Height to Bottom	= = =	0.0 #/ft 0.00 ft 0.00 ft
Load Type	=	Wind (W) (Service Level)
Wind on Exposed Stem (Strength Level)	=	0.0 psf



Adjacent Footing Load

=	0.0 lbs
=	0.00 ft
=	0.00 in
=	0.00 ft
	Spread Footing
=	0.0 ft
=	0.300
	= = =

Uniform Seismic Force = 49.000 Total Seismic Force = 343.000

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Project File: FND.ec6

Cantilevered Retaining Wall

LIC# : KW-06017913, Build:20.23.2.14 MULHERN & KULP STRUCTURAL ENGINEERING INC

DESCRIPTION: Garage Retaining Wall

Design Summary		St	em Construction		2nd	Bottom			
F.O.S. OF 1.1 ADEQUATE w/ SE	EISMIC A	PPLIED	Design Height Above Ftg		Stem OK	Stem OK			
Wall Stability Ratios			Wall Material Above "Ht"		Concrete	Concrete			
Overturning	=	1.29 Ratio < 1.5!	Design Method	_	SD	SD	SD	SD	
Slab Resis	ts All S	Sliding !	Thickness	=	8.00	8.00	02	02	
Global Stability	=	1.21	Rebar Size	=	# 5	# 5			
· · · · · · · · · · · · · · · · · · ·			Rebar Spacing	=	16.00	16.00			
Total Bearing Load	=	1,456 lbs	Rebar Placed at	=	Edge	Edge			
resultant ecc.	= ido mio	9.90 in	fb/FB + fa/Fa	_	0.056	0.468			
Soil Pressure @ Toe		945 psf OK	Total Force @ Section	_					
Soil Pressure @ Heel	=	0 psf OK	Service Level	lhs –					
Allowable	=	2,000 _{psf}	Strength Level	lbs –	330.4	1 302 0			
Soil Pressure Less	s Than	Allowable	MomentActual	100 -	000.1	1,002.0			
ACI Factored @ Toe	=	1,323 psf	Service Level	ft-# =					
ACI Factored @ Heel	=	0 psf	Strength Level	ft-# =	352.3	2,898.0			
Footing Shear @ Toe	=	9.3 psi OK	MomentAllowable	ft-# =	6,186.6	6,186.6			
Allowable	=	5.3 psi UK 75.0 psi	ShearActual						
Allowable	-	75.0 psi	Service Level	psi =					
Sliding Calcs			Strength Level	psi =	4.5	17.5			
Lateral Sliding Force	=	1.097.6 lbs	ShearAllowable	psi =	75.0	75.0			
5		.,	Anet (Masonry)	in2 =					
			Wall Weight	psf =	100.0	100.0			
			Rebar Depth 'd'	in =	6.19	6.19			
			Masonry Data						
Vertical component of active	e latera	al soil pressure IS	f'm	psi =					
considered in the calculation	n of so	il bearing pressures.	Fs	psi =					
			Solid Grouting	=					
Load Factors			Modular Ratio 'n'	=					
Building Code		4 000	Equiv. Solid Thick.	=					
		1.200	Masonry Block Type	=					
		1.000	Masonry Design Method	=	ASD				
Ealli, T		1.000	Concrete Data	:	0 500 0	0.500.0			
Soismic E		1.000		psi =	2,500.0	2,500.0			
		1.000	ГУ	psi =	00,000.0	00,000.0			

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Cantilevered Retaining Wall

LIC# : KW-06017913, Build:20.23.2.14 MULHERN & KULP STRUCTURAL ENGINEERING INC

DESCRIPTION: Garage Retaining Wall

Concrete Stem Rebar Area Details

2nd Stem	Vertical Reinforcing	Horizontal Reinforcing
As (based on applied moment) :	0.0133 in2/ft	
(4/3) * As :	0.0178 in2/ft	Min Stem T&S Reinf Area 0.513 in2
200bd/fy : 200(12)(6.1875)/60000 :	0.2475 in2/ft	Min Stem T&S Reinf Area per ft of stem Height : 0.192 in2/ft
0.0018bh : 0.0018(12)(8) :	0.1728 in2/ft	Horizontal Reinforcing Options :
		One layer of : Two layers of :
Required Area :	0.1728 in2/ft	#4@ 12.50 in #4@ 25.00 in
Provided Area :	0.2325 in2/ft	#5@ 19.38 in #5@ 38.75 in
Maximum Area :	0.8382 in2/ft	#6@ 27.50 in #6@ 55.00 in
Bottom Stem	Vertical Reinforcing	Horizontal Reinforcing
As (based on applied moment) :	0.1097 in2/ft	
(4/3) * As :	0.1463 in2/ft	Min Stem T&S Reinf Area 0.639 in2
200bd/fy : 200(12)(6.1875)/60000 :	0.2475 in2/ft	Min Stem T&S Reinf Area per ft of stem Height : 0.192 in2/ft
0.0018bh : 0.0018(12)(8) :	0.1728 in2/ft	Horizontal Reinforcing Options :
	==========	One layer of : Two layers of :
Required Area :	0.1728 in2/ft	#4@ 12.50 in #4@ 25.00 in
Provided Area :	0.2325 in2/ft	#5@ 19.38 in #5@ 38.75 in
Maximum Area :	0.8382 in2/ft	#6@ 27.50 in #6@ 55.00 in
Footing Data	Footing	Design Results
Toe Width =	2.50 ft	<u>Toe</u> <u>Heel</u>

	=	2	.50 IL
Heel Width	=	0	.67
Total Footing Width	=	3	.17
Footing Thickness	=	12	.00 in
Key Width	=	0	.00 in
Key Depth	=	0	.00 in
Key Distance from Toe	=	0	.00 ft
f'c = 2,500 psi	Fy =	60,0	000 psi
Footing Concrete Density	/ =	150	.00 pcf
Min. As %	=	0.00)18
Cover @ Top 2.00	@ E	3tm.=	3.00 in

		<u>10e</u>	Heel	
Factored Pressure	=	1,323	0 psf	
Mu' : Upward	=	2,625	0 ft-#	
Mu' : Downward	=	563	2 ft-#	
Mu: Design	=	2,062 OK	2 ft-#	OK
phiMn	=	2,500	OK - Flush	
Actual 1-Way Shear	=	9.31	5.34 psi	
Allow 1-Way Shear	=	40.00	75.00 psi	
Toe Reinforcing	=	None Spec'd		
Heel Reinforcing	=	Flush heel cond	dition. No reinfo	rcing required.
Key Reinforcing	=	None Spec'd		
Footing Torsion, Tu		=	0.00 ft-lbs	
Footing Allow. Torsion	ı, р	hi Tu =	0.00 ft-lbs	

If torsion exceeds allowable, provide supplemental design for footing torsion.

Other Acceptable Sizes & Spacings

Toe: phiMn = ph*5*lambda*sqrt(fc)*Sm

Heel: Flush heel condition. No reinforcing required.

Key: No key defined

Min footing T&S reinf Area	0.82	in2	
Min footing T&S reinf Area per foot	0.26	in2 /ft	
If one layer of horizontal bars:	<u>lf two lay</u>	ers of horiz	zontal bars:
#4@ 9.26 in	#4@1	8.52 in	
#5@ 14.35 in	#5@ 2	8.70 in	
#6@ 20.37 in	#6@4	0.74 in	

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Cantilevered Retaining Wall

LIC# : KW-06017913, Build:20.23.2.14 ML

MULHERN & KULP STRUCTURAL ENGINEERING INC

DESCRIPTION: Garage Retaining Wall

Summary of Overturning & Resisting Forces & Moments

		OV	ERTURNING			RESISTING		
Item		Force Ibs	Distance ft	Moment ft-#		Force lbs	Distance ft	Moment ft-#
HL Act Pres (ab water tb	D)	857.5	2.33	2,000.8	Soil Over HL (ab. water tbl)	2.2	3.17	7.0
HL Act Pres (be water tb Hydrostatic Force)			·	Soil Over HL (bel. water tbl) Water Table		3.17	7.0
Buoyant Force	=				Sloped Soil Over Heel =			
Surcharge over Heel	=				Surcharge Over Heel =			
Surcharge Over Toe	=				Adjacent Footing Load =			
Adiacent Footing Load	=				Axial Dead Load on Stem =			
Added Lateral Load	=				* Axial Live Load on Stem =			
Load @ Stem Above Soi	=				Soil Over Toe =			
Seismic Earth Load	=	240.1	3.50	840.4	Surcharge Over Toe =			
	=				Stem Weight(s) =	600.0	2.83	1,700.0
					Earth @ Stem Transitions =			
Total	=	1,097.6	O.T.M. =	2,841.2	Footing Weight =	475.5	1.59	753.7
					Key Weight =			
Resisting/Overturning Ratio = 1.29				Vert. Component =	378.5	3.17	1,199.9	
Vertical Loads used f	or Soi	I Pressure	= 1,456.	2 lbs	Total =	1,456.2	lbs R.M.=	3,660.5
					* Axial live load NOT included in	n total displa	yed, or used fo	roverturning

If seismic is included, the OTM and sliding ratios may be 1.1 per section 1807.2.3 of IBC.

Vertical component of active lateral soil pressure IS considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS considered in the calculation of Overturning Resistance.

Tilt

Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus 250.0 pci

Horizontal Defl @ Top of Wall (approximate only) 0.050 in

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe,

because the wall would then tend to rotate into the retained soil.

⁵ Axial live load NOT included in total displayed, or used for resistance, but is included for soil pressure calculation.

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